

June 9, 2021 Our File: 420023

City of Cambridge 50 Dickson Street Cambridge ON, N1R 5W8

Attention: Mr. Adam Ripper, P.Eng.

Re: Stormwater Management Brief – **REVISED** 355 Guelph Avenue and 11 Fletcher Circle City of Cambridge

Dear Mr. Ripper,

This letter has been prepared by GM BluePlan Engineering Limited to identify the stormwater management measures for the proposed residential development at 355 Guelph Avenue and 11 Fletcher Circle in the City of Cambridge. The 0.240-hectare site is bound by existing residential to the north and east, Fletcher Circle to the south and Guelph Avenue to the east. The 355 Guelph Avenue site is currently developed as a single-family residential lot. The 11 Fletcher Circle site is currently vacant.

Under existing conditions, runoff generated from a portion of the site sheetflows overland in a southeasterly direction to the existing swale on the 11 Fletcher Circle property, ultimately discharging to the existing DICB at the southeast corner of the property, and to the existing storm sewer on Fletcher Circle. The remainder of the site, consisting of the existing dwelling at 355 Guelph Avenue and landscaped areas, sheetflows overland to the east of the site towards the existing lots along Fletcher Circle. The subject site is part of the greater drainage catchment for the existing Mill Pond Subdivision and the existing Stormwater Management Facility at Shaw Avenue.

The Development Concept was prepared by Urbe Developments Inc. The topographic survey of the site was completed by J.D. Barnes Limited (dated March 25, 2020). The existing and proposed site details, along with the stormwater management controls, are shown on the Existing Conditions and Removals Plan, Site Servicing, and Site Grading Plan (GM BluePlan Engineering Limited).

PROPOSED DEVELOPMENT

The intent of the Owner at this time is to construct nine (9) townhouses, along with the associated asphalt driving and parking areas, and landscaped areas. Following development, runoff generated from the site will be directed to on-site swales, ultimately discharging to the existing municipal storm sewers on Fletcher Circle and to the existing stormwater management facility on Shaw Avenue. Runoff generated from the north portion of the site will continue to be directed towards the existing lots on Fletcher Circle, ultimately discharging to the existing stormwater management facility on Shaw Avenue.

STORMWATER MANAGEMENT CRITERIA

Based on the information provided by the City of Cambridge in the Pre-Consultation Comments, the criteria for the site is as follows:

1. Drainage from the subject properties was accounted for in the design of the adjacent Mill Pond subdivision and stormwater management facilities.

On-site quality control is required under post-development conditions for any portion of the site that exceeds the imperviousness of the stormwater management design for the Mill Pond Subdivision as identified below.

2. Peak flows from the post-development site for the 5-year and 100-year design storm events are to be attenuated to the design peak flows from the Mill Pond Subdivision, based on a runoff coefficient of 0.40 for the 355 Guelph Avenue property and a runoff coefficient of 0.55 for the 11 Fletcher Circle property.



The City of Cambridge Rainfall Distribution parameters and the total depth of rainfall used for the 5-year and 100-year design storm analysis are as follows:

	5-Year	100-Year
a =	1219.8	3015.1
b =	10.5	21.0
C =	0.823	0.870
r =	0.400	0.400
Duration (minutes)=	180.0	180.0
Maximum Intensity (mm/hr) =	127.834	177.123
Rainfall Depth (mm)=	48.647	89.669

Table No. 1: Rainfall Distribution Parameters

ALLOWABLE RELEASE RATES

As per the stormwater management criteria, the Mill Pond Subdivision stormwater management design utilized a runoff coefficient of 0.40 for 355 Guelph Avenue, and 0.55 for 11 Fletcher Circle. This following flow rates were calculated utilizing the Rational Method, utilizing a weighted average of the runoff coefficients identified for each property, and the individual property areas.

Table No. 2: Design Flows

	Runoff Coefficient	Site Area	5-Year Flow Rate	100-Year Flow Rate
355 Guelph Avenue	0.40	0.188-ha	0.026 m³/s	0.037 m³/s
11 Fletcher Circle	0.55	0.052-ha	0.010 m³/s	0.014 m³/s
Total Site	0.433	0.240-ha	0.037 m³/s	0.051 m³/s

Therefore, the allowable release rates for the site are as follows:

Table No. 3: Allowable Release Rate

	5-Year	100-Year
Allowable Release Rates	0.037 m³/s	0.051 m³/s

POST DEVELOPMENT CONDITIONS

For the post-development condition (illustrated in Figure No. 1), the 0.24-ha site was modelled as three (3) catchments.

Catchment 100 (0.15-hectares, 48% Impervious) represents the portion of the site which discharges uncontrolled to the Guelph Avenue and Fletcher Circle right-of-ways.

Catchment 200 (0.03-hectares, 45% Impervious) represents the back half of the roofs of the houses that front Guelph Avenue, as well as a portion of the rear yards of those lots.

Runoff generated from Catchment 200 will be convey to a subsurface infiltration gallery via inline drains. The subsurface infiltration gallery (18.5m long x 2.5m wide x 1.2m deep) has the capacity to infiltrate the 100-year design storm event from Catchment 200. Based on our history in the area, the native subsurface soils are a sandy silt till. We have conservatively estimated the infiltration rate at 5 mm/hour.



Catchment 300 (0.06-hectares, 46% Impervious) represents the back half of the roofs of the houses that front Fletecher Circle, as well as a portion of the rear yards of those lots.

Runoff generated from Catchment 300 will be convey to a subsurface infiltration gallery via inline drains. The subsurface infiltration gallery (33.5m long x 2.7m wide x 1.2m deep) has the capacity to infiltrate the 100-year design storm event from Catchment 300. Based on our history in the area, the native subsurface soils are a sandy silt till. We have conservatively estimated the infiltration rate at 5 mm/hour.

ROUTING

The hydrologic model MIDUSS was used to create the design storm runoff hydrographs and to route the hydrographs. A copy of the final printout of the hydrologic modelling is appended.

The results of the routing analysis are as follows:

	Available Capacity			Actual Capacity Used		
	Peak Flow m³/s	Storage Volume m ³	Storage Elevation m	Peak Flow m³/s	Storage Volume m ³	Storage Elevation m
Bottom of Stone	0.000	0.0	310.85			
5-Year				0.000	7.3	311.33
100-Year				0.000	17.8	312.01
Top of Stone	0.0001	18.5	312.05			
Tope of Grate	0.0001	18.6	312.55			

Table No. 4: Catchment 200 Infiltration Stage/Storage/Discharge Capacities

Table No. 5:	Catchment 300 Infiltration	Stage/Storag	ge/Discharg	e Capacities
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	Available Capacity			Actual Capacity Used		
	Peak Flow m³/s	Storage Volume m ³	Storage Elevation m	Peak Flow m³/s	Storage Volume m ³	Storage Elevation m
Bottom of Stone	0.000	0.0	310.45			
5-Year				0.000	14.9	310.95
100-Year				0.000	36.0	311.65
Top of Stone	0.0002	36.2	311.65			
Tope of Grate	0.0002	36.3	312.15			



In summary, the post-development flow rates from the site are as follows:

•		
	5-Year	100-Year
Catchment 100 (uncontrolled)	0.023 m³/s	0.047 m³/s
Catchment 200 (controlled)	0.000 m³/s	0.000 m³/s
Catchment 300 (controlled)	0.000 m³/s	0.000 m³/s
Total	0.023 m³/s	0.047 m³/s

Table No. 6: Post-Development Flow Rates

The following table compares the post-development condition flow rates to the existing condition release rates for the full range of design storm events.

	5-Year	100-Year
Allowable Release Rates	0.037 m³/s	0.051 m³/s
Post-Development Condition	0.023 m³/s	0.047 m³/s

Therefore, the 5 and 100-year post-development flow rates from the site have been attenuated to be less than the allowable release rates.

QUALITY CONTROL

The downstream Mill Pond subdivision and stormwater management facility was designed to treat flows from this site (area = 0.24 ha) at a runoff coefficient (RC) of 0.433, as noted above. As Catchments 200 and 300 are infiltrated on site, the only Catchment that will contribute to the downstream pond is Catchment 100, which is 0.15 ha at 48% impervious, which is equivalent to a runoff coefficient (RC) of approximately 0.54.

So, the pond was design for:	RC x Area = 0.433 x 0.24ha = 0.10

The site contributes: $RC \times Area = 0.54 \times 0.15ha = 0.08$

Therefore, on-site quality control will not be required as the proposed development is contributing less impervious area to the pond than it was designed for.

SEDIMENT AND EROSION CONTROLS

Silt fence will be installed along the property boundary in all locations where runoff will discharge from the site to adjacent lands. The silt fence will serve to minimize the opportunity for water borne sediments to be washed on to the adjacent properties.

Once catch basins have been relocated/installed, the grates will be wrapped with filter cloth. This feature will be maintained until all building and landscaping has been completed.

Inspection and maintenance of all silt fencing will start after installation is complete. The silt fence will be inspected on a weekly basis during active construction or after a rainfall event of 13 mm or greater. Maintenance will be carried out, within 48 hours, on any part of the facility found to need repair.

Once construction and landscaping has been substantially completed, the silt fence will be removed, any accumulated sediment will be removed and the landscaping will be completed.

After construction of the complete development, erosion and sediment transport will be minimal.



MAINTENANCE PLAN

To ensure that the stormwater management system continues to function as designed and constructed, we recommend that the following inspections and maintenance activities be completed on an annual basis:

- 1. Is there any noticeable damage to the asphalt and grassed swale (i.e. erosion, blockages)? If yes, complete any necessary repairs.
- 2. Inspect all ditch inlets, catch basins, and manholes. Remove and dispose of any accumulated sediment, trash/litter, debris (i.e. sediment, garbage, leaves, etc.).
- 3. Inspect all swales and overflow locations. Remove and dispose of any accumulated sediment, trash/litter, debris (i.e. sediment, garbage, leaves. etc.).
- 4. Is there any indication of a spill (i.e. frothy water, oily sheen on the water)? If yes, investigate, inform the appropriate agencies and complete the necessary clean-up and restoration.

Please note that any structures identified during the annual inspection to be worn, missing or damaged are to be repaired or replaced within 48 hours.

CONCLUSIONS

In summary, the preliminary stormwater management design for the development at 355 Guelph Avenue and 11 Fletcher Circle in the City of Cambridge is as follows:

- 1. Runoff generated from the site during the 5-year and 100-year design storm events has been attenuated to less than the allowable release rates from the site.
- 2. Quality control treatment for runoff generated from the site is provided through the existing stormwater management facility on Shaw Avenue, constructed as part of the Mill Pond Subdivision.

We trust this is the information you require at this time. If you have any questions or require additional information, please do not hesitate to call.

Yours truly,

GM BLUEPLAN ENGINEERING LIMITED

Per:

Patrick Grier, P.Eng. PG/ W:Kitchener\420-2020\420023 - 355 Guelph Avenue, Cambridge\GMBP Reports - SWM, FSR, Design Brief, etc\420023 SWM Brief - Revised - 2021-06-09.docx







355 GUELPH AVENUE, CAMBRIDGE Our File: 420023 May 27, 2021

Catchment 200: Proposed Infiltration Gallery

STORAGE VOLUME CALCULATIONS

-	ELEV (m)	INC D (m)	SURFACE AREA (Infil. Gall) (sq m)	INCR. STORAGE VOL (cu m)	ACCUM STORAGE VOL (cu m)	-
-	. ,	. ,	,	, , 		-
	310.85	0.00	46.25	0.00	0.00	Bottom of Stone
	311.05	0.20	46.25	3.08	3.08	j
	311.25	0.40	46.25	3.08	6.17	,
	311.45	0.60	46.25	3.08	9.25	
	311.65	0.80	46.25	3.08	12.33	j
	311.85	1.00	46.25	3.08	15.42	,
	312.05	1.20	46.25	3.08	18.50	Top of Stone
	312.40	1.55	0.60	0.04	18.54	, .
	312.55	1.70	0.60	0.04	18.58	T/G
	NFILTRATION		SIDE INFILTRATION	1		

			•••••••••••••••••••••••••••••••••••••••		
			ALL SIDES		
L(dw) =	18.5	m	L(dw) =	18.5	m
W(dw) =	2.5	m	W(dw) =	2.5	m
D(dw) =	1.20	m	D(dw) =		1.2 m
A(c) =	46.3	sq m	A(c) =	55.5	sq m
VOL(dw)=	55.5	cu m			
VOL(st)=	18.5	cu m			
K =	5	mm/hr	K =	5	mm/hr
=	1.39E-04	cm/s	=	1.39E-04	cm/s

ELEVATION	STAGE (m)	STORAGE (cu m)	INFILTRATION DISCHARGE (cu m/s)	TOTAL DISCHARGE (cu m/s)	_
310.85	0.00	0.00	0.00000	0.000000	Bottom of Stone
311.25	0.20	6.17 0.25	0.00009	0.000088	
311.65	0.80	12.33	0.00010	0.000111	
312.05	1.20	18.50	0.00012	0.000123	Top of Stone
312.40	1.70	18.58	0.00012	0.000123	T/G

355 GUELPH AVENUE, CAMBRIDGE Our File: 420023 May 27, 2021

Catchment 300: Proposed Infiltration Gallery

STORAGE VOLUME CALCULATIONS

-	ELEV	INC D	SURFACE AREA S (Infil. Gall)	INCR. STORAGE VOL	ACCUM STORAGE VOL	
	(m)	(m)	(sq m)	(cu m)	(cu m)	
-	310.45	0.00	90.45	0.0000	0.00	Bottom of Stone
	310.65	0.20	90.45	6.0300	6.03	
	310.85	0.40	90.45	6.0300	12.06	
	311.05	0.60	90.45	6.0300	18.09	
	311.25	0.80	90.45	6.0300	24.12	
	311.45	1.00	90.45	6.0300	30.15	
	311.65	1.20	90.45	6.0300	36.18	Top of Stone
	312.00	1.55	0.60	0.0377	36.22	
	312.15	1.70	0.60	0.0377	36.26	T/G
	FILTRATION		SIDE INFILTRATION			

		ALL	SIDES	
33.5	5 m	L(dv	/) =	33.5 m
2.7	'm	W(d	w) =	2.7 m
1.2	? m	D(dv	v) =	1.2 m
90.5	sq m	A(c)	=	108.54 sq m
108.5	cu m			
36.2	cu m			
5	mm/hr	Κ	=	5 mm/hr
1.39E-04	cm/s		=	0.000138889 cm/s
	33.5 2.7 1.2 90.5 108.5 36.2 5 1.39E-04	33.5 m 2.7 m 1.2 m 90.5 sq m 108.5 cu m 36.2 cu m 5 mm/hr 1.39E-04 cm/s	ALL 33.5 m L(dw 2.7 m W(d 1.2 m D(dw 90.5 sq m A(c) 108.5 cu m 36.2 cu m 5 mm/hr K 1.39E-04 cm/s	ALL SIDES 33.5 m L(dw) = 2.7 m W(dw) = 1.2 m D(dw) = 90.5 sq m A(c) = 108.5 cu m 36.2 cu m 5 mm/hr K = 1.39E-04 cm/s =

ELEVATION	STAGE (m)	STORAGE (cu m)	INFILTRATION DISCHARGE (cu m/s)	TOTAL DISCHARGE (cu m/s)	
310.45	0.00	0.0000	0.00000	0.000000	Bottom of Stone
310.65 310.85 211.05	0.20	6.0300 12.0600	0.00015	0.000146	
311.05 311.25 311.45	0.80	24.1200	0.00019	0.000186	
311.65	1.20	36.1800 36.2177	0.00023	0.000220	Top of Stone
312.15	1.70	36.2554	0.00023	0.000226	T/G

"		MIDUSS Output	>"
"		MIDUSS version	Version 2.25 rev. 473"
"		MIDUSS created	Sunday, February 07, 2010"
"	10	Units used:	ie METRIC"
"		Job folder:	C:\Users\pgrier\Documents\Work\"
"			420023 355 Guelph\2021-05-27"
"		Output filename:	420023_POST_5.out"
"		Licensee name:	gmbp"
"		Company	"
"		Date & Time last used:	5/27/2021 at 12:42:08 PM"
"	31 T	IME PARAMETERS"	
"	5.000	Time Step"	
"	180.000	Max. Storm length"	
"	1500.000	Max. Hvdrograph"	
	32 S	STORM Chicago storm"	
"	1	Chicago storm"	
	1219.800	Coefficient A"	
	10,500	Constant B"	
	0.823	Exponent C"	
	0.400	Expensive C Fraction B"	
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	1.000	Avimum intensity 1	27 834 mm/hr"
	Т	[otal denth	48 647 mm"
	6	005hvd Hydrograph extens	ion used in this file"
	33 0	ATCHMENT 100"	
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	100	Catchment 100"	
	18 000	% Imponyious"	
	48.000		
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	25 000	Pervious Area	
	25.000	Pervious length	
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	0.072	Impervious Area	
	25.000	Impervious length	
	2.000	Impervious slope	
	0.250	Pervious Manning 'n'	
	/5.000	Pervious Max.infiltration"	
	12.500	Pervious Min.infiltration"	
	0.250	Pervious Lag constant (hou	r's)
	5.000	Pervious Depression storag	e
	0.015	Impervious Manning 'n''	
	0.000	Impervious Max.intiltratio	n
	0.000	Impervious Min.infiltratio	n"
	0.050	Impervious Lag constant (h	ours)"
"	1.500	Impervious Depression stor	age"

"	0.02	.3 0.000	0.000	0.000 0	.m/sec"	
"	Catchment 10	0	Pervious	Impervious	Total Area	
"	Surface Area	l	0.078	0.072	0.150	hectare"
"	Time of cond	entration	13.431	1.802	4.065	minutes"
"	Time to Cent	roid	92.172	87.542	88.443	minutes"
"	Rainfall dep	th	48.647	48.647	48.647	mm"
"	Rainfall vol	ume	37.94	35.03	72.97	c.m"
"	Rainfall los	ses	38.282	2.167	20.947	mm"
"	Runoff depth	1	10.365	46.480	27.700	mm"
"	Runoff volum	ie	8.08	33.47	41.55	c.m"
"	Runoff coeff	icient	0.213	0.955	0.569	п
"	Maximum flow	I	0.006	0.021	0.023	c.m/sec"
"	40 HYDROGRAPH A	dd Runoff "				
"	4 Add Runof	f"				
"	0.02	.3 0.023	0.000	0.000"		
"	40 HYDROGRAPH C	Copy to Outf	low"			
"	8 Copy to C	utflow"				
"	0.02	3 0.023	0.023	0.000"		
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п	33 CATCHMENT 20	.9 0.000 19"	0.025	0:025		
	1 Triangula	r SCS"				
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	2 Horton ec	wation"				
	200 Catchmet	200"				
п	45,000 % Impervi	ous"				
п	0.030 Total Are	a"				
	25,000 Flow lens	rth"				
	2 000 Overland	Slone"				
	0 016 Pervious	Δrea"				
	25,000 Pervious	length"				
	2.000 Pervious	slone"				
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	12 500 Pervious	Min infilta	action"			
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"		0.050	Impervio	us Lag const	ant (hours))"		
"		1.500	Impervio	us Depressio	on storage"			
"			0.0	04 0.000	0.023	0.023 (.m/sec"	
"		Cat	chment 2	00	Pervious	Impervious	Total Area	п
"		Sur	face Are	а	0.016	0.013	0.030	hectare"
"		Tin	ne of con	centration	13.431	1.802	4.293	minutes"
"		Tin	ne to Cen [.]	troid	92.172	87.542	88.534	minutes"
"		Rai	infall de	pth	48.647	48.647	48.647	mm"
"		Rai	infall vo	lume	8.03	6.57	14.59	c.m"
"		Rai	infall lo	sses	38.282	2.167	22.030	mm"
"		Rur	noff dept	h	10.365	46.480	26.617	mm"
		Rur	loff volu	me	1.71	6.27	7.99	c.m"
		Rur	loff coef	ficient	0.213	0.955	0.547	
		Max	kimum flo	W	0.001	0.004	0.004	c.m/sec"
	40	HYE	DROGRAPH	Add Runoff '	1			
		4	Add Runo	ff "				
			0.0	04 0.004 	4 0.023	0.023"		
	54	PON	ND DESIGN	"	<i>,</i> "			
		0.004	Current	peak flow	c.m/sec"			
		0.005	larget of	UTTIOW C.	m/sec			
		8.0	Hydrogra	pn volume	C.m			
	2	9. 12 200	Minimum	T Stages	motho"			
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			310 850	0 000	0 000"			
			311,050	7.60E-05	3,080"			
			311,250	8.80E-05	6.170"			
			311.450	9.90E-05	9.250"			
			311.650	0.00011	12.330"			
			311.850	0.00012	15.420"			
"			312.050	0.00012	18.500"			
"			312.400	0.00013	18.540"			
"			312.550	0.00013	18.580"			
"		Pea	ak outflo	W	0.00	00 c.m/se	ec"	
"		Max	kimum lev	el	311.32	25 metre'	ı	
"		Max	kimum sto	rage	7.33	32 c.m"		
"		Cer	ntroidal	lag	15.75	55 hours"		
"			0.004	0.004	0.000	0.023 c.m/	'sec"	
"	40	HYD	OROGRAPH	Combine	1"			
"		6	Combine	п				
"		1	Node #"					
"			Combine"					
		Max	kimum flo	W	0.02	23 c.m/se	ec"	
		Нус	lrograph	volume	47.99	94 c.m"		
			0.0	04 0.004	0.000	0.023"		
	40	HYE	JROGRAPH	Start - New	Tributary"			

"	2	Start - New ⁻	Tributar	y"			
"		0.004	0.000	0.000	0.023"		
"	33	CATCHMENT 300"					
"	1	Triangular SO	CS"				
"	1	Equal length'					
"	2	Horton equat:	ion"				
"	300	Catchment 300	9"				
"	46.000	% Impervious'					
"	0.060	Total Area"					
"	25.000	Flow length"					
"	2.000	Overland Slop	be"				
"	0.032	Pervious Area	э"				
"	25.000	Pervious len	gth"				
"	2.000	Pervious slop	be"				
"	0.028	Impervious A	rea"				
"	25.000	Impervious le	ength"				
"	2.000	Impervious s	lope"				
"	0.250	Pervious Man	ning 'n'				
"	75.000	Pervious Max	.infiltr	ation"			
"	12.500	Pervious Min	.infiltr	ation"			
"	0.250	Pervious Lag	constan	t (hours)"			
"	5.000	Pervious Dep	ression	storage"			
"	0.015	Impervious Ma	anning '	n'"			
"	0.000	Impervious Ma	ax.infil [.]	tration"			
"	0.000	Impervious M:	in.infil [.]	tration"			
"	0.050	Impervious La	ag const	ant (hours)) "		
"	1.500	Impervious De	epressio	n storage"			
"		0.009	0.000	0.000	0.023 0	:.m/sec"	
"		Catchment 300		Pervious	Impervious	Total Area	
"		Surface Area		0.032	0.028	0.060	hectare"
		Time of concent	ration	13.431	1.802	4.215	minutes"
"		Time to Centroid	t s	92.172	87.542	88.503	minutes"
"		Rainfall depth	4	48.647	48.647	48.647	mm"
		Rainfall volume		15.76	13.43	29.19	c.m"
		Rainfall losses		38.282	2.167	21.669	mm"
		Runoff depth		10.365	46.480	26.978	mm"
		Runoff volume		3.36	12.83	16.19	c.m"
		Runoff coefficie	ent	0.213	0.955	0.555	" / "
	4.0	Maximum +low		0.002	0.008	0.009	c.m/sec"
	40	HYDROGRAPH Add I	Runott "				
	4	Add Runott "					
		0.009	0.009	0.000	0.023"		
	54	POND DESIGN"	C 1	<i>,</i>			
	0.009	Current peak	+TOM	c.m/sec"			
	0.005	larget outflo		m/sec"			
	16.2	Hydrograph vo	ornume	c.m"			
	9.	Number of sta	ages"				
	310.450	Minimum water	· Tevel	metre"			
	312.150	Maximum water	. TeAeT	metre"			
	310.450	Starting wate	er Tevel	metre"			

"		0 К	eep Desig	n Data: 1	= True; 0 =	= False"		
"			Level Di	scharge	Volume"			
"		3:	10.450	0.000	0.000"			
"		3:	10.650	0.00015	6.030"			
"		3:	10.850	0.00017	12.060"			
"		3:	11.050	0.00019	18.090"			
"		3:	11.250	0.00021	24.120"			
"		3:	11.450	0.00023	30.150"			
"		3:	11.650	0.00023	36.180"			
"		3:	12.000	0.00023	36.220"			
"		3:	12.150	0.00023	36.260"			
"		Peak	outflow		0.00)0 с.	m/sec"	
"		Maxi	mum level		310.94	15 me	tre"	
"		Maxi	mum stora	ge	14.93	36 c.	m''	
"		Cent	roidal la	g	16.43	3 hou	rs"	
"			0.009	0.009	0.000	0.023	c.m/sec"	
"	40	HYDR	OGRAPH	Combine	1"			
"		6 C	ombine "					
"		1 No	ode #"					
"		C	ombine"					
"		Maxi	mum flow		0.02	23 c.	m/sec"	
"		Hydro	ograph vo	lume	60.72	26 c.	m''	
"		2	0.009	0.009	0.000	0.0	23"	
"	40	HYDR	OGRAPH	Confluence	1"			
"		7 C	onfluence	п				
"		1 No	ode #"					
"		C	ombine"					
"		Maxi	mum flow		0.02	23 c.	m/sec"	
"		Hydro	ograph vo	lume	60.72	26 c.	m"	
"		,	0.009	0.023	0.000	0.0	00"	
"	38	STAR	T/RE-STAR	T TOTALS 1	"			
"		3 R	unoff Tot	als on EXI	Т"			
"		Tota	l Catchme	nt area			0.240	hectare"
"		Tota	l Impervi	ous area			0.113	hectare"
"		Tota	1 % imper	vious			47.125"	
"	19	EXIT						

"		MIDUSS Output	>"
"		MIDUSS version	Version 2.25 rev. 473"
"		MIDUSS created	Sunday, February 07, 2010"
"	10	Units used:	ie METRIC"
"		Job folder:	C:\Users\pgrier\Documents\Work\"
"			420023 355 Guelph\2021-05-27"
"		Output filename:	420023_POST_100.out"
"		Licensee name:	gmbp"
"		Company	"
"		Date & Time last used:	5/27/2021 at 12:30:03 PM"
"	31 T	IME PARAMETERS"	
"	5.000	Time Step"	
"	180.000	Max. Storm length"	
"	1500.000	Max. Hydrograph"	
"	32 S	TORM Chicago storm"	
"	1	Chicago storm"	
"	3015.100	Coefficient A"	
"	21.000	Constant B"	
"	0.870	Exponent C"	
"	0.400	Fraction R"	
	180.000	Duration"	
	1.000	Time step multiplier"	
	M	aximum intensity	177.123 mm/hr"
	Т	otal depth	89.669 mm"
	6	100hvd Hvdrograph exter	sion used in this file"
	33 C	ATCHMENT 100"	
	1	Triangular SCS"	
"	1	Equal length"	
"	2	Horton equation"	
	100	Catchment 100"	
	48,000	% Impervious"	
"	0.150	Total Area"	
	25.000	Flow length"	
"	2.000	Overland Slope"	
	0.078	Pervious Area"	
	25.000	Pervious length"	
	2.000	Pervious slope"	
	0.072	Impervious Area"	
	25.000	Impervious length"	
	2.000	Impervious slope"	
	0.250	Pervious Manning 'n'"	
	75.000	Pervious Max.infiltration	п
	12.500	Pervious Min.infiltration	"
	0.250	Pervious Lag constant (ho	urs)"
	5.000	Pervious Depression stora	ge"
	0.015	Impervious Manning 'n'"	0-
	0.000	Impervious Max.infiltrati	on"
	0.000	Impervious Min.infiltrati	on"
	0.050	Impervious Lag constant (hours)"
"	1.500	Impervious Depression sto	rage"

"	0.0	0.00	0.000	0.000	c.m/sec"	
"	Catchment 1	.00	Pervious	Impervious	Total Area	н
"	Surface Are	a	0.078	0.072	0.150	hectare"
"	Time of cor	centration	8.974	1.582	4.141	minutes"
"	Time to Cer	ntroid	93.374	86.798	89.074	minutes"
"	Rainfall de	epth	89.669	89.669	89.669	mm"
"	Rainfall vo	lume	69.94	64.56	134.50	c.m"
"	Rainfall lo	sses	47.202	2.757	25.868	mm"
"	Runoff dept	:h	42.467	86.912	63.801	mm"
"	Runoff volu	ıme	33.12	62.58	95.70	c.m"
"	Runoff coef	ficient	0.474	0.969	0.712	"
"	Maximum flo)W	0.022	0.032	0.047	c.m/sec"
"	40 HYDROGRAPH	Add Runoff				,
"	4 Add Rund	off "				
"	0.0	0.04	7 0.000	0.000"		
"	40 HYDROGRAPH	Copy to Out	flow"			
п	8 Copy to	Outflow"	-			
"	0.0	947 0.04 [°]	7 0.047	0.000"		
"	40 HYDROGRAPH	Combine	1"			
"	6 Combine	"	-			
п	1 Node #"					
п	Combine"					
п	Maximum flo)W	0.0	47 c.m/se	•د"	
	Hydrograph	volume	95.7	01 c.m"		
	nyar ograph o o	47 0 04 [.]	7 0 047	0 047"		
	40 HYDROGRAPH	Start - New	Tributary"	0.047		
	2 Start -	New Tributa	rv"			
	2 50010	147 0.00	, 0 0.047	0.047"		
п	33 CATCHMENT 2	947 0100 900"	0 0:04/	0.047		
	1 Triangul	ar SCS"				
п	1 Foual le	ngth"				
	2 Horton e	auation"				
	200 Catchmet	200"				
п	45,000 % Imperv	ious"				
	0.030 Total Ar	rea"				
	25,000 Flow ler	ogth"				
	2 000 Overland	Slone"				
	0 016 Pervious	: Δrea"				
	25,000 Pervious	length"				
	2 000 Pervious	slone"				
п	0 013 Impervic	us Area"				
	25 000 Impervie	us length"				
	23.000 Impervice 2 000 Tenenvice	us slone"				
	2.000 impervious 0.250 Denvious	Manning 'n				
	75 000 Denvious	May infilt	ration"			
	12 500 Fervious	Min infilt	nation"			
	$\begin{array}{cccc} 12.500 & Fervious \\ 0.250 & Donvious \\ \end{array}$	$= 1 \Rightarrow a = constant$	nt (house)"			
	5 000 Ponvious	Depression	stonado"			
		Me Manning	'n'"			
		us namitig	" ltpation"			
	e.eee impervic	us max. 11171.				

"		0.000	Impervio	ous Min.infi	ltration"			
"		0.050	Impervio	ous Lag cons [.]	tant (hours))"		
"		1.500	Impervio	ous Depressi	on storage"			
"			0.0	0.00	0 0.047	0.047 (.m/sec"	
"		Ca	atchment 2	.00	Pervious	Impervious	Total Area	
"		Su	urface Are	a	0.016	0.013	0.030	hectare"
"		Ti	ime of con	centration	8.974	1.582	4.346	minutes"
"		Ti	ime to Cen	itroid	93.374	86.798	89.256	minutes"
"		Ra	ainfall de	pth	89.669	89.669	89.669	mm"
"		Ra	ainfall vo	lume	14.80	12.11	26.90	c.m"
"		Ra	ainfall lo	sses	47.202	2.757	27.201	mm"
		Rι	unoff dept	:h	42.467	86.912	62.468	mm"
		Rι	unoff volu	ime	7.01	11.73	18.74	c.m"
		Ru	unoff coef	ficient	0.474	0.969	0.697	
		Ma	aximum flo	W	0.005	0.006	0.009	c.m/sec"
	40	H١	/DROGRAPH	Add Runoff				
		4	Add Runo	off "				
		_	0.0	0.00	9 0.047	0.047"		
	54	P(DND DESIGN	l"	/ "			
		0.009	Current	peak tiow	c.m/sec			
		0.005	larget o	OUTTION C	.m/sec			
		18./	Hyurogra	ipn volume	C.m			
		212 200	Minimum	T Stages	mot no"			
		212.200	Marimum	water level	metre			
		212 200	Stanting	water level	1 metre			
		012.200		ign Data: 1	$- True \cdot 0 -$	- Falso"		
		0		Discharge	Volume"	- 18136		
			310 850	0 000	0 000"			
			311.050	7.60E-05	3.080"			
			311.250	8.80E-05	6.170"			
			311.450	9.90E-05	9.250"			
			311.650	0.00011	12.330"			
"			311.850	0.00012	15.420"			
"			312.050	0.00012	18.500"			
"			312.400	0.00013	18.540"			
"			312.550	0.00013	18.580"			
"		Pe	eak outflo	W	0.00	00 c.m/se	ec"	
"		Ma	aximum lev	'el	312.00	06 metre'	ı	
"		Ma	aximum sto	rage	17.82	21 c.m"		
"		Ce	entroidal	lag	26.53	11 hours"		
"			0.009	0.009	0.000	0.047 c.m/	'sec"	
"	40	H١	/DROGRAPH	Combine	1"			
"		6	Combine	п				
"		1	Node #"					
"			Combine"					
		Ma	aximum flo	W _	0.04	47 c.m/se	ec"	
		Ну	/drograph	volume	105.52	25 c.m"		
			0.0	0.00	9 0.000	0.047"		
	40	H١	URUGRAPH	Start - New	Tributary"			

"		2	Start - New Tr	ibutar	ry"				
"			0.009	0.000	0.000	0.047"			
"	33	CA	CHMENT 300"						
"		1	Triangular SCS						
"		1	Equal length"						
"		2	Horton equatio	n"					
"		300	Catchment 300"						
"	46.	000	% Impervious"						
"	0.	060	Total Area"						
"	25.	000	Flow length"						
"	2.	000	Overland Slope						
"	0.	032	Pervious Area"						
"	25.	000	Pervious lengt	h"					
"	2.	000	Pervious slope						
"	0.	028	Impervious Are	a"					
"	25.	000	Impervious len	gth"					
"	2.	000	Impervious slo	pe"					
"	0.	250	Pervious Manni	ng 'n'					
	75.	000	Pervious Max.i	nfiltr	ration"				
	12.	500	Pervious Min.i	nfiltr	ration"				
	0.	250	Pervious Lag c	onstar	nt (hours)"				
"	5.	000	Pervious Depression storage"						
	0.	015	Impervious Man	ning	'n'"				
"	0.	000	Impervious Max	.infi	ltration"				
"	0.	000	Impervious Min	.infi	ltration"				
"	0.	050	Impervious Lag	const	tant (hours))"			
	1.	500	Impervious Dep	ressio	on storage"				
			0.019	0.000	0.000	0.047	:.m/sec"		
		Cat	tchment 300		Pervious	Impervious	Total Area		
		Sur	rface Area		0.032	0.028	0.060	hectare"	
		Tir	ne of concentra	tion	8.974	1.582	4.277	minutes"	
		Tir	ne to Centroid		93.373	86.798	89.195	minutes"	
		Rai	infall depth		89.669	89.669	89.669	mm	
		Rai	Infall volume		29.05	24.75	53.80	c.m.	
		каз	Infall losses		47.202	2./5/	26.757	mm.	
		Rur	loff depth		42.467	86.912	62.912	mm ^a	
		Rur	nott volume		13.76	23.99	3/./5	c.m"	
		Rur	iott coetticien	τ	0.4/4	0.969	0.702		
	40	Max	KIMUM TIOW		0.009	0.012	0.019	c.m/sec	
	40	HYL	Add Dunoff "	потт					
		4		0 010	0 000	0 047"			
			0.019	0.015	9 0.000	0.047			
	54	PUI 010	ND DESIGN	1	a				
	0.	00E 0TA	Tangot outflow	TOM	c.m/sec				
	ح	כשש ד ד	Undergreen and	C.					
	3	/./	Numbon of ctor	ullie oc"	C.III				
	210	э. 150	Minimum wotoo		mot no"				
	210.	150	Mavimum water		metre"				
	210	150	Stanting water						
	210.	470	Starting water	телет					

		0	Keep Desi	gn Data: 1	1 = Tr	rue: 0 =	= Fal	se"		
		•	Level D	ischarge	Vo	lume"				
			310,450	0.000	0	.000"				
			310.650	0.00015	6	.030"				
			310.850	0.00017	12	.060"				
			311.050	0.00019	18	.090"				
			311.250	0.00021	24	.120"				
			311,450	0.00023	30	150"				
			311.650	0.00023	36	.180"				
			312,000	0.00023	36	.220"				
			312.150	0.00023	36	260"				
		Pea	ak outflow	0100010		0.00	90	c.m/sec"		
		Max	ximum leve	1		311.64	45	metre"		
		Max	ximum stor	- age		36.03	30	c.m"		
		Cer	ntroidal l	age		28.56	91	hours"		
			0.019	0.019	0	.000	0.0	47 c.m/sec"		
	40	HYI	DROGRAPH	Combine	1"			,		
		6	Combine "		_					
		1	Node #"							
		_	Combine"							
		Max	ximum flow			0.04	17	c.m/sec"		
		Hvo	drograph v	olume		124.05	52	c.m"		
			0.01	9 0.01	19	0.000	-	0.047"		
	40	HY	DROGRAPH	Confluend	ce	1"				
	-	7	Confluenc	e "						
		1	Node #"	-						
		_	Combine"							
		Max	ximum flow			0.04	17	c.m/sec"		
		Hvo	drograph v	olume		124.05	52	c.m"		
		0,019 0,047				0.000	_	0.000"		
	38	ST	ART/RE-STA	RT TOTALS	1"					
"		3	Runoff To	tals on EX	KIT"					
		Tot	tal Catchm	ent area				0.240	he	ectare"
		Tot	Total Impervious area					0.113	he	ectare"
		Tot	tal % impervious					47.125"		
"	38	ST	ART/RE-STA							
		3	Runoff Totals on EXIT"							
"		Tot	tal Catchm	ent area				0.240	he	ectare"
"		Tot	tal Imperv	ious area				0.113	he	ectare"
"		Tot	tal % impe	rvious				47.125"		
"	19	EX	IT"							