SERVICING & STORM WATER MANAGEMENT REPORT

FOR

200 DUNDAS STREET SOUTH

CAMBRIDGE, ONTARIO

August 09, 2021

Prepared by:

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1.0 INTRODUCTION

The purpose of this report is to present the storm water management, connections for sanitary sewage disposal and water distribution for the proposed development.

The subject site is located south of Dundas Street South as shown in Figure 1.

Figure 1 - Site Location Plan

2.0 EXISTING SITE CONDITIONS AND TOPOGRAPHY

The site has approximately 0.30 ha area. Currently the site has existing commercial single storey building and vacant land with mostly hardscaped area (gravel/asphalt).

A legal and topographic survey has been prepared by Lejan Land Surveying Inc. dated June 03, 2021 which identifies the site as part of Lots 5 & 6, Concession 10, North Dumfries in the City of Cambridge, Regional Municipality of Waterloo.

The existing site sheet drains towards Dundas Street. The elevations on the site ranges from 293.46 m at the north west corner to 292.24 m at the north east corner. The existing grades around the site are proposed to be matched at the boundary limits.

3.0 PROPOSED DEVELOPMENT

The proposed development consisits of a multi storey commercial/residential building with parking area. The proposed building ground floor level is kept at 293.50 m for Commercial 2 & 3 and 293.20 m for Commercial 1 (Refer drawing C102). Proposed site servicing, grading and erosion control plans are submitted separately as full size drawings with this report

4.0 EXISTING SERVICES & STORM SEWER CONNECTION

Existing record drawings obtained from City of Cambridge and Region of Waterloo show that the sanitary, storm and watermain services are available on Dundas Street for service connection.

The information of existing services is summarized in table below;

TABLE 1 – EXISTING SERVICES SUMMARY

Service	Size	Location
Watermain	200mm & 300 mm (City Owned) 450 mm (Region Owned)	Dundas Street
Storm Sewer	300 mm (Region Owned)	Dundas Street
Sanitary Sewer	200mm	Dundas Street

Refer Drawing C101 for location and details of exsiting services

5.0 STORM WATER MANAGEMENT AND METHODOLOGY

The following SWM criteria is applicable for the site;

Quantity Control
The quantity control is pre to post development flows for all storms (2,5,10,25,50 & 100) year.
Quality Control
The Quality control to MOE Enhanced level (80% removal of suspended solids)
Erosion and Sediment Control
Adequate measures are to be implemented to minimize the transportation of sediments out of the construction area.

5.1 Quantity Control

The site is mainly divided into catchment areas A1 and A2 based on proposed development and grading. The catchment areas ``A1" (0.24 ha) contains building and parking, whereas the catchment area ``A2``(0.06 ha) is flowing uncontrolled in pre and post development conditions due to grading constraints and is excluded from storm water management calculations.

The pre and post development land use with drainage catchments are shown in Figure DR01 and DR02 Appendix A.

The Pre and post development landuse breakdown and runoff coefficients are shown in Table 2 & Table 3 below**.**

TABLE 2- PRE DEVELOPMENT RUNOFF COEFFICIENT

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient
Landscape	0.003	0.25
Gravel	0.023	0.90
Hardscape	0.212	0.90
Overall	0.238	0.89

TABLE 3- POST DEVELOPMENT RUNOFF COEFFICIENT

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient
Landscape	0.008	0.25
Gravel	0.076	0.90
Hardscape	0.152	0.90
Overall	0.238	0.88

The pre and post development impervious levels remain the same and there will be no increase in peak flows as a result of proposed development. Therefore, quantity control is not required.

The Rainfall intensities shall be calculated in accordance with City of Cambridge IDF curves. The “Modified Rational Method” is used to estimate flows from the drainage areas.

The pre and post development flows are calculated in Table B3, Appendix B, which shows that post development flows are less than predevelopment flows.

5.2 Quality Control

To address quality and spills control from site, an oil & grit separator is proposed at the storm manhole STMH2 before connection to existing storm sewer. The proposed stormceptor will treat the impervious area up to 80% TSS removal for Level 1 water quality protection.

5.3 Minor Storm Drainage

The storm sewer network designed for 5 year strom event is proposed to convey the site drainage and connect to an existing 300 mm sewer. A direct connection is proposed to the

exsisting storm sewer on Dundas Street. The drawing C101 shows the proposed site storm network.

5.4 Major System Drainage

The overland flow will not impact the building since the grading of the site ensures storm flows greater than 100 years will be able to flow overland through the site without any impact to proposed buildings and adjacent site.

The overland flow route is shown on Drawing C102.

6.0 SERVICING DESIGN CRITERIA

The following design criteria has been used for water demand and sanitary flow calculations for the proposed development.

TABLE 4 – WATER & SANITARY DESIGN CRITERIA

WATER SYSTEM DESIGN CRITERIA	
Residential	225 Lpcd
Max Day Factor	1.44
Peak Flow	Max Day + Fire Flow
Fire Flow Calculation Method	FUS Method
SANITARY SYSTEM DESIGN CRITERIA	
Residential Generation Rate	275 Lpcd
Commercial Generation Rate	75 Lpcd
Peaking Factor	Use Harmon Formula
Extraneous Flows	0.25 L/s/ha
POPULATION DENSITY	
Residential Units	1.83 Persons per unit
Commercial	9.3 Persons /m^2

Design Criteria as per:

- *Region of Waterloo and Area Municipalities Design Guidelines and Supplemental Specifications for Municipal Servicing (DGSSMS), Januray 2018*
- *Engineering Standard and Development Manual, Cambridge, October 2013*

6.1 Water

A 150 mm dia water service is proposed for the new building. The proposed connection is shown on drawing C101.

The total average daily demand for the proposed building is calculated as follows:

Water Demand Calculations

Residential Units = 40 units

Population= 1.83 persons per unit = 73 persons

Residential Demand = 225 x 73 = 16,425 l/day = 0.19 l/sec

Commercial Area = 442 m^2

Commercial Demand = 442/9.3 x 75 = 0.041 l/sec

Total Average Water Demand = 0.19 + .041 = 0.231 l/sec

Maximum daily demand = Average demand x Peaking Factor

Maximum day demand = 0.231 l/s x 1.44= 0.332 l/s

Fire demand as per FUS calculations = 100 l/sec (Refer Table B4- Appendix B)

Max day + Fire = 0.332+100 = 100.332 l/sec = 6020 l/min.

As per pre consultation comments, the subject property is currently located in the Cambridge Zone 1 pressure zone (CAM1) with an existing HGL of 322 mASL.

Cambridge Zone 1 will be undergoing adjustments to the HGL. The porject site will be serviced from Pressure Zone Cambridge 1a, and the future expected hydraulic grade line of 349.5 mASL for ultimate design. The anticipated timeline for the HGL adjustment is by end of 2023.

The available pressure 349.5 mASL which corresponds to 80 psi is adequate for the proposed development.

6.2 Sanitary

A 200 mm dia sanitary service with a control manhole is proposed for the new building. The proposed sanitary network is shown on drawing C101.

The total sanitary flow is calculated as follows;

Residential Units = 40 units

Population= 1.83 persons per unit = 73 persons

Residential Flow = 275 x 73 = 20,075 l/day = 0.232 l/sec

Commercial Area = 442 m^2

Commercial Flow = 442/9.3 x 75 = 0.041 l/sec

Total Average Sanitary Flow = 0.232+0.041 = 0.273 l/sec

Total Sanitary Peak Flow = 0.273 X 4.0 = 1.092 l/sec

Extraneous Flow = 0.25 X 0.30 = 0.075 l/sec (Site Area = 0.30 ha)

Design Flow = 1.092+ 0.075 = 1.17 l/sec.

7.0 EROSION AND SEDIMENT CONTROL

An erosion and sediment control strategy will be implemented during the construction to mitigate the transportation of silt from the site. Drawing C103 shows silt fence and sediment control measures.

To prevent construction-generated sediments from entering the storm sewer or leaving the site by overland flow, the following measures should be implemented with regular inspection and maintenance;

- Management of construction activities in a manner to minimize disturbed area and duration of soil disturbance;
- Provision of a mud mat construction access to minimize sediment on adjacent municipal road;
- Installation of drain inlet protection at each catch basin and storm manhole cover within the construction site and downstream of the construction access on the adjacent municipal road;
- Installation and maintenance of silt fences (OPSD 219.130 or equivalent) around the perimeter of any construction/disturbed areas;
- Periodically removal of sediments accumulated behind silt fences or sediment protection when 50% of its individual design capacity has been reached
- Dust control measures should be followed during construction.
- Erosion and sediment control practices to be decommissioned after paving, landscaping or other stabilization measures and restoration of disturbed areas have been completed.

8.0 CONCLUSIONS

- Quantity control is not required as the pre and post development impervious levels remain the same and there will be no increase in peak flows as a result of redevelopment.
- Quality control will be acheived through provision of oil/grit separator.
- Overland flow route through the site ensures that major overland flows are safely carried through the site towards Major Street.
- Sediment and erosion control measures shall be implemented, such as the installation of mud mat, temporary silt fence and filter fabric at the existing catch basins.

We trust you will find this submission complete and in order. Should you have any questions, please contact the undersigned.

Respectfully Submitted,
Jain Infrastructure Consultants Ltd.

Yasar Ayub, P. Eng.
August 09, 2021

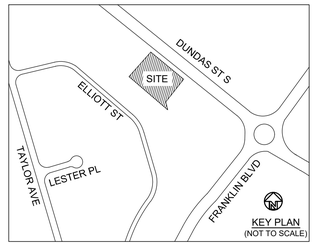
Usman Arif
Project Designer

Appendix A
Figures
DR01 Pre Development Drainage Areas
DR02 Post Development Drainage Areas

LEGEND:

- CATCHMENT AREA BOUNDARY
- OVERLAND FLOW ROUTE
- CATCHMENT AREA No.
- CATCHMENT AREA IN HECTARES.
- WEIGHTED RUN-OFF COEFFICIENT

A1 / 0.08 / 0.89



TRUE NORTH

CONSTRUCTION NORTH

A.K.A. KING'S HIGHWAY NO. 8
A.K.A. REGIONAL ROAD NO. 8
D U N D A S S T R E E T S O U T H
P.I.N. 03824-0028 (LT)

CENTRE LINE OF ROAD

N50°31'00"W REFERENCE BEARING

PORTION D PLAN 511

PORTION D PLAN 255

A1 / 0.24 / 0.89

A2 / 0.06 / 0.74

1 STY. CONCRETE BLOCK BUILDING No. 160

2 STY. BRICK DWELLING No. 200 DS.= 293.86

2 STY. BRICK BUILDING No. 246

SHED

DECK

CONCRETE PAD

PORCH

GAS METER

HYDRO METER

ROW OF TREES

P.I.N. 03842-0037 (LT)

P.I.N. 03842-0038 (LT)

P.I.N. 03842-0039 (LT)

P.I.N. 03842-0103 (LT)

P.I.N. 03842-0104 (LT)

P.I.N. 03842-0105 (LT)

P.I.N. 03842-0106 (LT)

P.I.N. 03842-0107 (LT)

P.I.N. 03842-0108 (LT)

LOT 6 CONCESSION 10 LOT 5

PART 3 PLAN 67R2837

PART 4 PLAN 67R2837

PART 5 PLAN 67R2837

DESIGN CONSULTANT:

JAIN

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CAMBRIDGE CANADA
It's all right here

SITE PLAN CONTROL
APPLICATION FILE NO.: SP41/19

LICENCED PROFESSIONAL ENGINEER
Y.AYUB
AUG 09,21
PROVINCE OF ONTARIO
21-530

200 DUNDAS ST.S

200 DUNDAS STREET SOUTH, CAMBRIDGE ON, N1R 8A8

Project: A20006

PURELAND INVESTMENTS INC.

Date Plotted: 2021-08-06 5:39:26 PM
Drawn by: C.C.
Scale: 1:150

REV #	DATE	DESCRIPTION
1	08-09-2021	ISSUED FOR ZONING APPROVAL

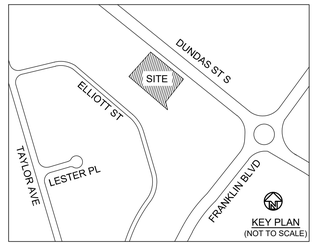
PRE DEVELOPMENT DRAINAGE AREAS

DR01

LEGEND:

- CATCHMENT AREA BOUNDARY
- OVERLAND FLOW ROUTE
- CATCHMENT AREA No.
- CATCHMENT AREA IN HECTARES.
- WEIGHTED RUN-OFF COEFFICIENT

A1 / 0.08 / 0.89



TRUE NORTH

CONSTRUCTION NORTH

DESIGN CONSULTANT:

JAIN

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Email: yayub@jainconsultants.com

CAMBRIDGE CANADA
It's all right here

SITE PLAN CONTROL APPLICATION FILE NO.: SP41/19

LICENCED PROFESSIONAL ENGINEER
Y.AYUB
AUG 09,21
PROVINCE OF ONTARIO
21–530

200 DUNDAS ST.S

Project:

200 DUNDAS STREET SOUTH, CAMBRIDGE ON, N1R 8A8

A20006 PURELAND INVESTMENTS INC.

Date Plotted: 2021-08-06 5:39:31 PM
Drawn by: C.C.
Scale: 1:150

REV #	DATE	DESCRIPTION
1	08-09-2021	ISSUED FOR ZONING APPROVAL

POST DEVELOPMENT DRAINAGE AREAS

DR02

Appendix B

Table B1 - Pre Development Land Use & Runoff Coeffiecients
Table B2 - Post Development Land Use & Runoff Coeffiecients
Table B3 – Pre & Post Development Flows
Table B4 – Fire Flow Calculations

TABLE B1. Land use Breakdown and Composite Runoff Coefficients Calculations Existing Conditions

Date: 06-Aug-21

Project: 200 Dundas Street South, Cambridge, ON

Designer UA

Checker YA

TABLE B1.1 CATCHMENT AREA A1

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient	A x R
Landscape	0.003	0.25	0.001
Gravel	0.023	0.90	0.020
Hardscape	0.212	0.90	0.191
Overall	0.238	0.89	0.212

TABLE B1.2 CATCHMENT AREA A2 (Uncontrolled)

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient	A x R
Landscape	0.014	0.25	0.004
Gravel	0.010	0.9	0.009
Hardscape	0.034	0.9	0.031
Overall	0.058	0.74	0.043

** Catchment Area "A2 =0.058" is excluded from SWM calculations as it is uncontrolled in pre and post development due to existing grades around the site*

TABLE B2. Land use Breakdown and Composite Runoff Coefficients Calculations Proposed Conditions

Date: 06-Aug-21

Project: 200 Dundas Street South, Cambridge, ON

Designer UA

Checker YA

TABLE B2.1 CATCHMENT AREA A1

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient	A x R
Landscape	0.008	0.25	0.002
Building	0.078	0.90	0.070
Hardscape	0.152	0.90	0.137
Overall	0.238	0.88	0.002

TABLE B2.2 CATCHMENT AREA A2 (Uncontrolled)

Proposed Land Use/ Cover	A, Area (hectares)	R, Runoff Coefficient	A x R
Landscape	0.045	0.25	0.011
Hardscape	0.014	0.9	0.012
Overall	0.058	0.40	0.023

** Catchment Area "A2 =0.058" is excluded from SWM calculations as it is uncontrolled in pre and post development due to existing grades around the site*

TABLE B3 PEAK FLOWS CALCULATION USING RATIONAL METHOD
EXISTING AND PROPOSED CONDITIONS

Date: 06-Aug-21

Project: 200 Dundas Street South, Cambridge, ON **Designer** UA

Checker YA

TABLE B3.1 Intensity-Duration-Frequency Parameters, City of Cambridge

$I = A/(T_c+B)^C$

Return Period	IDF Parameters			Intensity (mm/hr)
	A	B	C	Tc 10 min
2 year	573.1	5	0.761	73.0
5 year	1219.8	10.5	0.823	101.6
10 year	1728.6	14	0.849	116.4
25 year	2226.9	17	0.865	128.7
50 year	2640	19	0.866	142.9
100 year	3015.1	21	0.870	152.0

TABLE B3.2 Peak Flows - Existing Conditions

Existing Condition	Area (ha.)	R	A x R		
Area A1	0.238	0.89	0.21		
T c = 10 minutes					
Storm Event					
2 year	**5 year**	**10 year**	**25 year**	**50 year**	**100 year**
Intensity (mm/hr)					
73.0	101.6	116.4	128.7	142.9	152.0
Peak Flow (cms)					
0.043	0.060	0.069	0.076	0.084	0.090

TABLE B3.3 Peak Flows - Proposed Condition

Proposed Condition	Area (ha.)	R	A x R		
Area A1	0.238	0.88	0.21		
T c = 10 minutes					
Storm Event					
2 year	**5 year**	**10 year**	**25 year**	**50 year**	**100 year**
Intensity (mm/hr)					
73.0	101.6	116.4	128.7	142.9	152.0
Peak Flow (cms)					
0.042	0.059	0.068	0.075	0.083	0.088

TABLE B4 **FIRE FLOW CALCULATION as per FIRE UNDERWRITERS SURVEY (1999)**

PROJECT: 200 Dundas Street South, Cambridge, ON

1. Fire Flow Equation

$$F = 220\ C\ \sqrt{A}$$

where F is the required fire flow [LPM]
C is the coefficient determined by type of construction [unitless]
A is the total protection area [sq.m]

2. Architecture Information

Type of Construction	Ordinary Construction	
Fire Rating	Combustible	
Sprinkler Provided (Y/N)	No	
Total Floor Area [sq.m]	1161	Largest Floor + 25% of two adjoining floors
Coefficient, C [1]	1.0	Ordinary
Fire Flow, F [LPM]	7496	

3. Occupancy Reduction

Occupancy Adjustment	1.00
Fire Flow, F [LPM]	7496

4. Sprinkler Reduction

Sprinkler Reduction	0.30
Sprinkler Reduction [LPM]	2249

5. Exposure Adjustment

North	0%
East	5%
South	5%
West	5%
Total	**15%**
Exposure Adjustment [LPM]	1124

6. Required Fire Flow, Duration & Volume

Fire Flow, F [LPM]	7496	
Sprinkler Reduction [LPM]	2249	
Exposure Adjustment [LPM]	1124	
Required Fire Flow [LPM]	6372	
Required Fire Flow [LPM]	**6000**	Round to nearest 1000
Required Fire Flow [LPS]	**100**	
Req. Duration of Fire Flow [hrs]	2	
Req. Storage [cubic.m]	720	

Appendix C

Stormceptor

Stormceptor® EF

Stormceptor® EF Overview

imbrium®

About Imbrium® Systems

Imbrium® Systems is dedicated to protecting Canada's waterways. Based on our knowledge and experience in the Canadian stormwater industry, we have the ability to provide the most effective stormwater treatment technologies that capture and retain harmful pollutants from urban runoff before it enters our streams, rivers, lakes, and oceans.

Imbrium's engineered treatment solutions have been third-party tested and verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol to ensure performance in real-world conditions as designed. Our team of highly skilled engineers and partners provide the highest level of service from design to installation and long-term maintenance.

By working with Imbrium and our partners, you can expect superior treatment technology, unparalleled customer service, compliance with local stormwater regulations, and cleaner water. To find your local representative, please visit **www.imbriumsystems.com/localrep**.

Learn About the Stormceptor® EF

Go online and watch our animation to learn how the Stormceptor EF works. The animation highlights important features of the Stormceptor EF including:

- Functionality
- Applications
- Inspection and Maintenance

To view the Stormceptor EF animation, visit **www.imbriumsystems.com/stormceptoref**

Stormceptor® EF

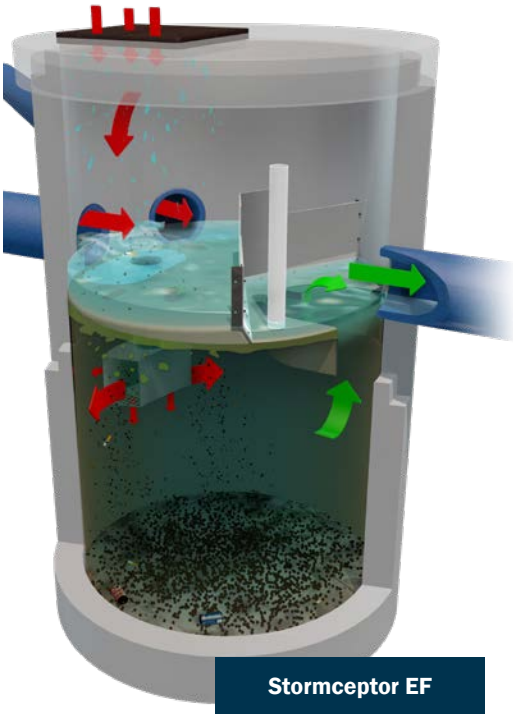
A CONTINUATION AND EVOLUTION OF THE MOST GLOBALLY RECOGNIZED OIL GRIT SEPARATOR (OGS) STORMWATER TREATMENT TECHNOLOGY

Stormceptor EF effectively targets sediment (TSS), free oils, gross pollutants and other pollutants that attach to particles, such as nutrients and metals. Stormceptor EF's independently tested and verified, patent- pending treatment and scour prevention platform ensures pollutants are captured and contained during all rainfall events.

Stormceptor EF also offers design flexibility in one platform, accepting flow from a single inlet pipe, multiple inlet pipes, and from the surface through an inlet grate. Stormceptor EF can also accommodate a 90-degree inlet to outlet bend angle, and tailwater conditions.

Ideal Uses

- Sediment (TSS) removal
- Hydrocarbon control and hotspots (Stormceptor EF)
- Debris and small floatables capture
- Pretreatment for filtration, detention/retention systems, ponds, wetlands, and bioretention
- Retrofit and redevelopment projects

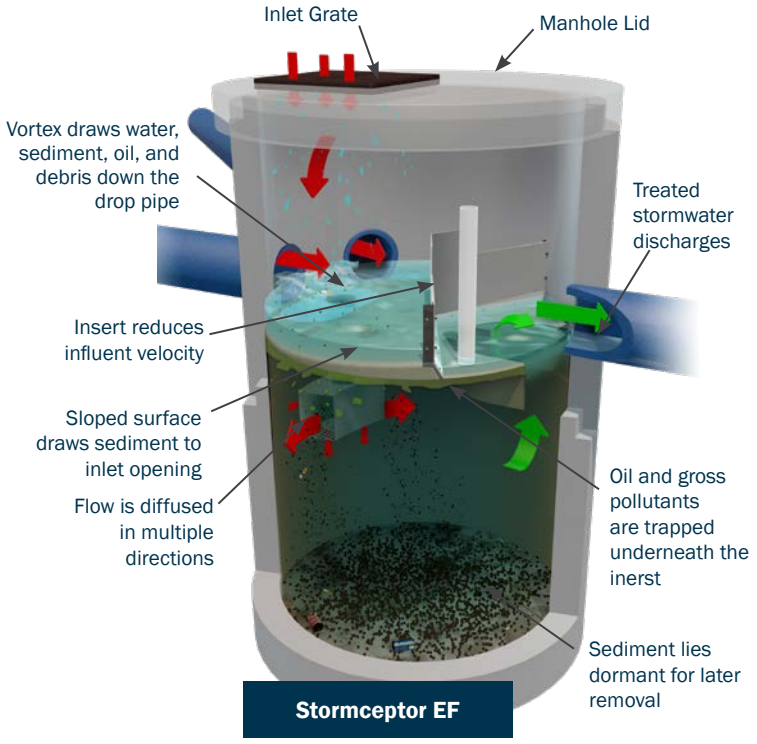


Stormceptor EF

Stormceptor EF and Stormceptor EFO have been verified in accordance with ISO 14034 Environment Management - Environmental Technology Verification (ETV) protocol.

How the Stormceptor® EF Works

- Flow enters the Stormceptor through one or more inlet pipes or an inlet grate.
- A specially designed insert reduces influent velocity by creating a pond upstream of the weir, allowing sediments to begin settling.
- Swirling flow sweeps water and pollutants across the sloped insert surface to the drop pipe, where a strong vortex draws water, sediment, oil, and debris down the drop pipe cone and into the lower chamber.
- Flow exits the drop pipe through two large rectangular openings, while also diffusing through perforations in multiple directions. This reduces stream velocities and increases pollutant removal efficiency while preventing resuspension and washout of previously captured pollutants.
- Floatables, such as oil and gross pollutants, rise up and are trapped beneath the insert.
- Sediment settles to the sump.
- Treated stormwater discharges to the top side of the insert downstream of the weir, where it exits through the outlet pipe.
- During intense storm events excess influent passes over the weir and exits through the outlet pipe. The pond continues to separate sediment from all incoming flows, while full treatment in the lower chamber continues at the maximum flow rate, without scour of previously captured pollutants.

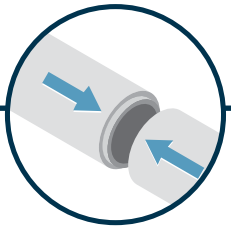


* Fiberglass system is an option

Stormceptor® EF Features & Benefits

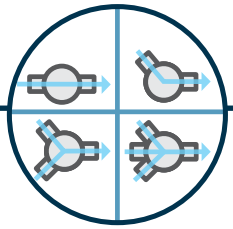
EASY TO INSTALL

Small footprint saves time and money with limited disruption to your site.



SEAMLESS

Minimal drop between inlet and outlet pipes makes Stormceptor ideal for retrofits and new development projects.

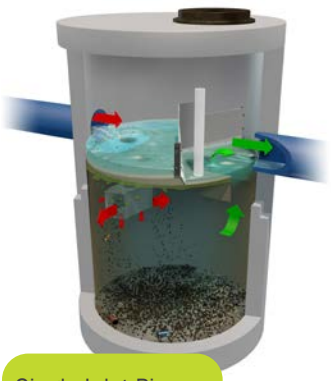


FLEXIBLE

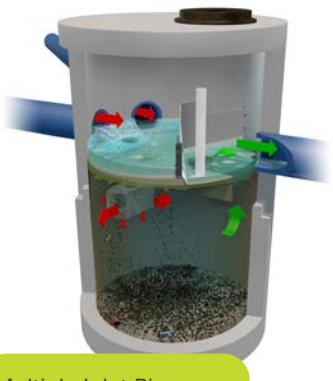
Multiple inlets can connect to a single unit. Can be used as a bend structure.

FEATURES	BENEFITS
Patent-pending enhanced flow treatment and scour prevention technology	Superior, third-party verified performance
Third-party verified light liquid capture and retention (EFO version)	Proven performance for fuel/oil hotspot locations
Functions as bend, junction or inlet structure	Cost savings and design flexibility
Minimal drop between inlet and outlet	Site installation ease
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade

Stormceptor® EF Standard Configurations

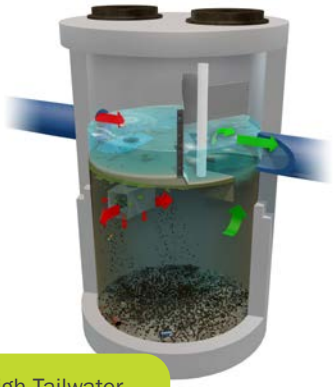


Single Inlet Pipe



Multiple Inlet Pipes

Grate Inlet



High Tailwater

OPTIONS & ACCESSORIES

The following options and accessories are available for specific functions and site conditions:

- **Tailwater/Submerged Site** – For sites with standing water during dry weather periods, weir modifications can be implemented to ensure optimal performance.
- **Additional Sediment Storage Volume** – For sites with high pollutant loads or remote sites, additional sediment storage volume can easily be added.
- **Oil Alarm** – To mitigate spill liability, a monitoring system can be employed to trigger a visual and audible alarm when an oil or fuel spill occurs.
- **Additional Oil Capture** – A draw-off tank can be incorporated to increase spill storage capacity.
- **High Load** – Standard design loading is CHBDC or AASHTO H-20. Specialized loading can be designed to withstand very high loadings typical of airports and port facilities.
- **Lightweight** – Sites that required lightweight or above ground units are available as complete fiberglass systems.

Optional Oil Alarm

For any of these options or accessories, please contact your Stormceptor representative for design assistance.

Stormceptor® EFO

Accidents and spills happen, whether it is a fueling station, port, ndustrial site, or general hot spot with daily vehicle traffic. Protect the environment and your site from potentially costly clean-up, remediation, litigation and fines with the Stormceptor EFO configuration.

The Stormceptor EFO has been third-party tested to ensure oil capture, and retention during high flow events. The hydraulics of the Stormceptor EFO have been optimized to enhance oil and hydrocarbon capture.

STORMCEPTOR EFO – HYDROCARBON SPILL PROTECTION

- Stormceptor EFO configuration has been third-party performance tested for safe oil capture and retention.
- Patent-pending technology ensures captured oil and sediment are retained even during the largest rain events, for secure storage, environmental protection and easy removal.
- Stormceptor EFO provides double wall containment for captured hydrocarbons.
- Stormceptor EFO is ideal for gas stations, fuel depots, ports, garages, loading docks, industrial sites, fast food locations, high-collision intersections and other hotspots with spill-prone areas.
- Stormceptor EFO can accommodate an optional oil alarm and additional storage to increase spill storage capacity.

Stormceptor® Inspection & Maintenance

Conducted at grade, the Stormceptor EF design makes inspection and maintenance an easy and inexpensive process. Once maintained, the Stormceptor EF is functionally restored as designed, with full pollutant capture capacity.

MAINTENANCE RECOMMENDATIONS:

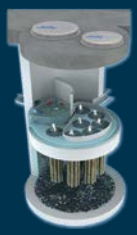
- Inspect every six months for the first year to determine the pollutant accumulation rate.
- In subsequent years, inspections can be based on observations or local requirements.
- Inspect the unit immediately after an oil, fuel or chemical spill. A licensed waste management company should remove oil and sediment, and dispose responsibly.

Stormceptor maintenance is performed at grade with a standard vacuum truck

ADDITIONAL SOLUTIONS

FILTERRA® BIORETENTION

The Filterra® Bioretention System is an engineered biofiltration device with components that make it similar to bioretention in pollutant removal and application, but has been optimized for high volume/flow treatment in a compact system.



JELLYFISH® FILTER

The Jellyfish® Filter is a stormwater treatment technology featuring pretreatment and membrane filtration in a compact stand-alone treatment system that removes a high level and a wide variety of stormwater pollutants.

LEARN MORE

- Access project profiles, photos, videos, and more online at **www.imbriumsystems.com/stormceptoref.**

REQUEST DESIGN ASSISTANCE

- Call us at (888) 279-8826 or 301-279-8827 to talk to one of our engineers for technical support or design assistance.

START A PROJECT

- Submit your system requirements on our product Design Worksheet at **www.imbriumsystems.com/pdw.**

FIND A LOCAL REPRESENTATIVE

- Visit **www.imbrumsystems.com/localrep** for contact information for your local Imbrium representative.

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Imbrium® Systems is an engineered stormwater treatment company that designs and manufactures stormwater treatment solutions that protect water resources from harmful pollutants. By developing technologies to address the long-term impact of urban runoff, Imbrium ensures our clients' projects are compliant with government water quality regulations. For information, visit www.imbriumsystems.com or call +1 416-960-9900.

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By Canadians, for Canadians.